

Original Article

Retrospective Assessment of Respirable Quartz Exposure for a Silicosis Study of the Industrial Sand Industry

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Abstract

Background: In 2016, the OSHA PEL for crystalline silica was reduced, renewing interest in evaluating risk of silicosis from occupational exposures. The industrial sand industry, which deals with high-purity quartz sands, is the setting for a current epidemiologic investigation of silicosis risk and progression. In support of that investigation, respirable quartz (RQ) exposures were retrospectively estimated for 67 workers with silicosis and 167 matched control workers from 21 industrial sand plants, in which some started work as early as 1929.

Methods: A job exposure matrix (JEM) was constructed by integrating a modern (post-1970) RQ exposure database containing more than 40 000 measurements with archival particle count exposure data from a 1947 survey. A simulation algorithm was used to develop a conversion factor to convert the archival particle count data into modern measures of RQ by randomly generating 100 000 virtual dust particles of varying diameters corresponding to the size distributions of 14 archival particle size distribution samples. The equivalent respirable mass and particle counts of the virtual particles were calculated, totalled, and ratioed to derive the conversion factor. The JEM was integrated with individual job histories to calculate average and cumulative exposure for each case and control. Multiple exposure estimates were derived for unprotected exposures as well as for exposures adjusted for estimated respiratory protective equipment use and efficiency.

Results: The mean of the count to respirable mass conversion factors derived from 14 archival particle size samples was 157 $\mu\text{g m}^{-3}$ per mppcf (SD: 42; range: 96–263) with no statistical difference across process areas (drying, screening, vibrating, binning, bulk loading, bagging), $P = 0.29$. The JEM demonstrated an industry-wide decrease in prevailing exposures to RQ of up to about 2 orders of

magnitude from the distant (1929) to the recent (2012) past. Unadjusted cumulative exposures for cases and controls were statistically different ($P < 0.001$) with respective medians (range) of 3764 $\mu\text{g m}^{-3}$ year (221–25 121) and 1595 $\mu\text{g m}^{-3}$ year (0–16 446). Adjustment of exposure for use of respiratory protection showed modest reductions in estimated exposure: median adjusted cumulative exposures assuming a protection factor of 5 were 86% and 77% of the unadjusted values for cases and controls, respectively.

Conclusions: The industrial sand industry offers a unique setting for examination of silicosis risk because of the high silica content of industrial sand and a long history of radiographic silicosis surveillance of industry workers. However, the great majority of silicosis cases in this industry are found among former workers and are associated with exposures occurring in the distant past, which necessitates extensive retrospective exposure assessment and increases the likelihood of exposure misclassification. Nonetheless, the estimated cumulative exposures for silicosis cases and controls in this work were significantly different, with the median cumulative exposure for cases being more than twice that of their matched controls.

Keywords: silicosis; exposure assessment; industrial sand; quartz; JEM; respiratory protection; simulation

Introduction

The industrial sand industry produces commercial grade silica (quartz) sands and ground silica flour for use in glass-making, foundries, paints and plastics, and oil and gas “fracking” operations. Industrial sands are extracted from deposits of sandstones or granular sands. Hard compact sandstones are mined by drilling and blasting operations to release sandstone boulders. These are subsequently reduced to manageable size by heavy mobile equipment in the quarry. The rocks are then transported to automated crushers in the processing plant. Soft friable sandstone is often hydraulically mined with high-pressure water cannon. Loose sand aggregates are extracted from deposits by power shovel or dredge.

The recovered granular sands may be wet processed to remove clays, calcite, iron, and other undesirable constituents, sometimes with size-separation through wet screening. The cleaned sand is then drained and dried. In the past, steam coil dryers were common; these were gradually replaced by rotary kiln and fluid bed dryers. Dried sand may be packaged directly or may be further size segregated through dry screening or air separation. In some plants, processed sand is pulverized in ball or rod mills to produce ground silica (silica flour), which consists of very fine crystalline silica particles in size fractions down to 5 μm . Sand and silica flour are bagged or bulk loaded into railcars, hopper cars, or trucks for shipment.

Industrial sands are characterized by very high content of crystalline silica. Excessive exposure to airborne respirable silica particles can result in silicosis, a progressive fibrotic lung disease (ACGIH, 2010). Silica exposure has also been linked to an increase in risk of lung cancer and kidney disease (Hughes *et al.*, 2001; McDonald

et al., 2001; Steenland, 2001; McDonald *et al.*, 2005) and the International Agency for Research on Cancer (IARC, 1997) has classified crystalline silica as a human carcinogen. The OSHA Permissible Exposure Limit for respirable quartz (RQ) in general industry had been approximately equal to 100 $\mu\text{g m}^{-3}$ since 1970 but was reduced to 50 $\mu\text{g/m}^3$ in June 2016.

Most of the epidemiologic information on risk of silicosis, lung cancer and other diseases associated with workplace exposure to crystalline silica derives from retrospective mortality studies of workforces from the distant past when exposures were much higher than today, use of respiratory protective equipment was either nonexistent or ineffective, and exposure data was sparse, and prior to the 1970s, measured in outdated particle count concentrations. The industrial sand industry has been the setting for several such epidemiologic investigations, (Hughes *et al.*, 2001; McDonald *et al.*, 2001; Steenland and Sanderson, 2001; McDonald *et al.*, 2005) and the work described herein was performed in support of a new examination of the radiographic prevalence and progression of silicosis among industrial sand workers dating back to 1929 (Vacek *et al.*, 2018).

This study was approved by Solutions IRB, a private, fully accredited Institutional Review Board and by the Human Research Protections Office/IRB of Tulane University.

Methods and materials

Data sources

Two member companies of the National Industrial Sand Association (NISA) provided employee information,

chest radiographs, work histories, and exposure measurements used in this work and the companion epidemiologic study (Vacek *et al.*, 2018). The initial study cohort included 1902 male production workers from 40 plants in 22 states. To identify silicosis cases, the latest chest X-ray for each worker was reviewed and classified by two or three NIOSH B readers using the ILO's International Classification of Radiographs for Pneumoconioses (International Labor Office, 2011). Films graded at a median profusion classification of 1/0 or greater were considered diagnostic of silicosis. Earlier films for each silicosis case were then read to determine first onset of silicosis. The initial cohort yielded 67 cases of radiographically diagnosed silicosis from 21 plants: 11 from Company A and 10 from Company B. The cases were matched with two to three controls each, randomly selected from among men employed at the same plant and born within 3 years of the case with no radiographic indication of silicosis prior to the date of diagnosis of the case, for a total of 167 controls and a combined total of 234 workers in the final group for which exposure assessment was conducted. The researchers involved in the exposure estimation were blinded to subject identity and case/control status.

Work histories for the final group of cases and controls were compiled by the participating companies under the coordination of one of the authors (REG). Company A's human resource records were mostly electronic, but for Company B, much of the earlier data were abstracted from paper copy. The companies developed the job histories by in-house review of their personnel, employment, and medical records, supplementing this information as needed by discussions with workers and supervisors. The job histories included date of initial hire with the company along with job title and department or work area and subsequent jobs and dates held until the study cut-off date (2013) or termination of employment.

Job histories received from the companies were reviewed and each entry in a worker's job history was coded for the specific job and plant corresponding to those in the job exposure matrix (JEM).

Exposure measurements

Beginning in the early 1970s, the two companies participating in this study have collected to date over 49 000 samples for RQ using 10-mm nylon cyclone with a membrane filter for the analysis of collected quartz via X-ray diffraction. In addition to this database, quantitative data from archival consultant reports and the Mine Safety and Health Administration's online database (<https://arlweb.msha.gov/drs/drshome.htm>; last accessed 6 July 2018) were used to reconstruct exposures, particularly

for exposures occurring before the 1970s and for certain plants that had been in operation under different ownership before being acquired by the participating companies. Also, available information was acquired on plants' process flow, breakdowns of jobs and departments/areas, history of major process or engineering changes with an emphasis on those that may have altered dust concentrations in the workplace, and use of respiratory protective equipment (RPE).

Development and application of the JEM

For each of the 21 plants having a case and controls, a separate JEM was developed for the period beginning with earliest date of hire of case or control workers, to the termination of employment or study cut-off date (2013), using an approach similar to that employed in our previous mortality studies of the industrial sand industry (Rando *et al.*, 2001; McDonald *et al.*, 2005). The JEM was linked to the specific job histories of the participating workers to calculate yearly exposures for each individual. These were then used to compute cumulative and average exposures to RQ, as well as other exposure metrics.

A dictionary of job codes for each plant was developed after careful review of the respective job history profiles, and current and historical plant and process information. In a few situations where cross-over among job titles and tasks within plant departments was a common occurrence, a department-wide job code and corresponding average concentration was assigned for all workers involved, regardless of job title.

Estimates of average exposure to RQ for each job code were computed as the arithmetic mean of the data over time segments in which the concentrations were judged to be stable. The arithmetic mean was used because chronic inhalation exposures are physiologically integrated in a linear fashion and the inhaled exposure dose can be negatively biased when using geometric mean exposure concentration in dose response analyses (Seixas *et al.*, 1988; Crump, 1998). Temporal trends or changes in the exposures were first identified by graphical examination of the data and then evaluated using traditional statistical tests for significance (*t*-test, ANOVA) on the log-transformed data. Identified changes in exposure were correlated with any known dates of changes in process, work practices, and dust controls. When no statistically significant changes or trends in exposure were identified, the mean of the data across all times for a given job was used as the exposure estimate.

Individual exposure measurements that were below the limit of detection ($\sim 6 \mu\text{g m}^{-3}$) were flagged as being censored and the grouped data were analyzed using the

log-probit regression, maximum likelihood estimation, or beta substitution techniques to obtain statistically robust estimates of the geometric mean and geometric standard deviation. The arithmetic mean of the data was then calculated using the minimum variance unbiased estimator (MVUE). These analytical procedures were performed with IH DataAnalyst software using the program's censored data analysis routines (Exposure Assessment Solutions, Inc.; Morgantown, West Virginia).

For reported jobs in which either no specific sampling was ever done, no specific information on the job's tasks was available (for example, "labor" and "utility"), or for time segments of an individual's job history with missing job information, RQ exposures were assumed to be equal to the overall mean of the estimates for all production jobs in the facility.

To estimate RQ exposures prior to the starting date of the modern database (~1970), the history of a given job and facility identified probable dates for any likely changes in dust concentration based on process changes, dust controls, etc. After that date, concentration estimates derived from the modern exposure database were extrapolated back in time to the point of the change. Preceding such changes, exposure estimates were based on archival data from a series of reports submitted to NISA by Professor Theodore Hatch through the Industrial Hygiene Foundation of America between 1947 and 1955 (Hatch *et al.*, 1947; Hatch, 1954; Hatch and Wellington, 1955). The 1947 report contained approximately 500 dust measurements from 19 separate facilities processing industrial sand. Of the 19 facilities, data from 3 plants in this study could be specifically identified and used for past exposure estimation. For the other plants in this study, dust measurement data were averaged by production areas/tasks across all 19 plants.

Conversion of archival exposure measures

Hatch's 1947 survey data were collected using Greenburg Smith impingers with enumeration of collected particles by bright field microprojector microscopy. The resulting dust measurements were nonspecific and were reported in units of million particles per cubic foot (mppcf). For use in this study, the Hatch particle count concentration data had to be converted to the equivalent modern unit system of $\mu\text{g m}^{-3}$ RQ.

In similar studies of other industries such as the Vermont granite sheds (Montgomery *et al.*, 1991 and Ayer *et al.*, 1973), conversion factors have been obtained directly from side-by-side samples collected by impinger and by respirable cyclone sampler. This approach requires access to plants and processes that are representative of past conditions when the archival data

were collected; however, with plant modernization and implementation of dust exposure controls over time, this is typically not possible. The industrial sand industry has changed dramatically over time, so a computational approach must be taken to develop the conversion factor. In our previous work, (Rando *et al.*, 2001) this computation was based on 14 archival particle size samples collected in various areas in several industrial sand plants (Severns, 1979). These samples were collected on membrane filters with a 10-mm nylon cyclone preseparator and analyzed by oil-immersion microscopy with 400–500 particles in each sample counted and classified into nine size categories ranging between 0.3 and 4.8 μm . Additionally, for each sample the count median diameter (CMD) and geometric standard deviation (GSD) of the particle size distribution were estimated by graphical analysis (Table 1).

We estimated the corrected number concentration of particles in each of the nine size categories by accounting for the sampling efficiency of the cyclone/filter (ϵ_c). The collection/analysis efficiency of the impinger/microscope (ϵ_i) was then applied to the corrected number concentration to determine the expected number concentration from an impinger collection and analysis of that sample. The

Table 1. Particle count to respirable mass conversion factors for industrial sand dust derived from archival particle size data (Severns, 1979) using the simulation algorithm.

Area	Original size distribution of respirable dust		CF ^a ($\mu\text{g m}^{-3}$ mppcf ⁻¹)
	CMD (μm)	GSD	
Dryers	0.36	2.1	136
	0.55	2.5	263
	0.55	2.1	181
	0.41	2.1	146
Screen	0.44	1.9	115
Air Sizers	0.46	2.3	202
	0.44	2.0	134
Vibrators	0.37	2.2	157
	0.39	2.2	162
Binroom	0.56	2.0	160
Bulkloading	0.36	2.3	186
Bagging	0.30	2.2	137
	0.30	2.1	121
	0.33	1.7	96
Overall (mean \pm SD)			157 \pm 42

CMD: count median diameter; GSD: geometric standard deviation; CF: conversion factor. ^aNo significant differences in CF between areas. ANOVA, $P = 0.29$.

original particle counts in each size category were then converted to equivalent respirable mass concentration assuming spherical silica particles. The number and mass contributions in each size category were summed and ratioed to determine the conversion factor for that sample.

Our previous computational algorithm yielded a conversion factor of $276 \mu\text{g m}^{-3}$ per mppcf which is in the upper range of conversion factors reported by others for various types of mineral dusts and is significantly greater than those developed for siliceous dusts which generally range around a value of $125 \mu\text{g m}^{-3}$ per mppcf (Supplementary Table S2, available at *Annals of Work Exposures and Health*). Our original computational algorithm had several limitations: imprecision for size categories with low particle counts, assignment of collection efficiency of the category median particle size to all particles in a given size category, truncating the counts at $4.8 \mu\text{m}$ thus excluding respirable particle mass of larger particles, and assuming that all particles in the sample were silica with a density of 2.65 g cm^{-3} .

In this present work, the computational algorithm for the conversion factor has been updated with a stochastic approach using computer simulations based on the particle size distributions of the samples. The simulation algorithm entailed generation of 100 000 individual virtual particles with projected area diameter of the i th particle ($d_{p,i}$) randomly chosen from a log-normal distribution of particle sizes having the CMD and GSD of the corresponding archival sample. The simulations were run in Microsoft Excel using the RiskAMP Monte Carlo Simulation add-in (Structured Data, LLC; San Francisco, California; www.riskamp.com). Virtual particles with random values of $\ln(d_{p,i})$ were generated using the 'NormalValue' function in RiskAMP which returns a value randomly chosen from the normal distribution with the input mean ($\ln \text{CMD}$) and standard deviation ($\ln \text{GSD}$).

For each of the virtual particles, their equivalent respirable mass was calculated according to equation (1) where $d_{p,i}$ is particle diameter, ρ_i is the particle density, and M_i is the particle mass. The density of each virtual particle was randomly chosen from among the following values: 1.8 g cm^{-3} (black carbon/soot), 2.6 g cm^{-3} (kaolin), 2.65 g cm^{-3} (quartz), and 2.7 g cm^{-3} (calcite). This approximates the composition of airborne particulate matter in industrial sand plants as reported by Hatch *et al.*, (1947).

$$M_i = \frac{\pi d_{p,i}^3}{6} \rho_i \quad (1)$$

Next, for each virtual respirable particle, the corresponding number of particles of such diameter was determined

by dividing the count of one by the collection efficiency of the cyclone/filter assembly; that is, the single virtual particle would have been part of a family of such sized particles in the air sample, only one of which was collected. For example, if the cyclone/filter collection efficiency for a particular sized virtual particle is 0.1 (or 10%) then there would actually have been on average a total of 10 such particles in the whole sample prior to separation by the cyclone. The corresponding equivalent particle count by impinger/microscopy then is the product of the adjusted particle count and the efficiency of measurement by impinger collection/microscopy. Combining these two adjustments yields equation (2), where N_i is equivalent particle count of the i th virtual particle by impinger collection and microscopy, $\varepsilon_{i,i}$ is the impinger/microprojector measurement efficiency for virtual particle i , and $\varepsilon_{c,i}$ is its cyclone/filter collection efficiency:

$$N_i = \frac{\varepsilon_{i,i}}{\varepsilon_{c,i}} \quad (2)$$

The 10-mm cyclone/filter collection efficiency, ε_c , has been shown to meet the 1984 ACGIH respirable dust sampling convention reasonably well (ACGIH, 1984; Tsai and Shih, 1995):

...those particles that penetrate a separator whose size collection efficiency is described by a cumulative lognormal function with a median aerodynamic diameter (d_{AE}) of $3.5 \mu\text{m} \pm 0.3 \mu\text{m}$ and with a geometric standard deviation of $1.5 (\pm 0.1)$.

Hence, the cyclone collection efficiency, ε_c , was calculated for each virtual particle according to equation (3) where Φ is the cumulative normal distribution function, and $d_{AE,i}$ is the aerodynamic equivalent diameter of the i th particle ($d_{AE,i} = d_{p,i} (\rho_i)^{1/2}$):

$$\varepsilon_{c,i} = 1 - \Phi \left(z = \frac{\ln(d_{AE,i} / GM)}{\ln(\text{GSD})} \right) \quad (3)$$

Calculation of ε_c according to equation (3) was performed using the 'LOGNORM.DIST' function in Microsoft Excel, with input values of 1.253 and 0.405 ($\ln(GM = 3.5 \mu\text{m})$) and ($\ln(\text{GSD} = 1.5)$), respectively. This applied to simulation particles with d_{AE} less than or equal to $10 \mu\text{m}$. The corrected particle count of simulation particles greater than $10 \mu\text{m}$ was set to zero because the conversion factor was extremely sensitive to the presence of such large particles owing to the cubic relationship of mass and diameter and such large particles would have been removed from the sample by the cyclone pre-separator.

The impinger/microprojector measurement efficiency, ε_p , was set to zero for virtual particles with $d_{p,i}$ less than

0.75 μm ($d_{AE,i} < 1.2 \mu\text{m}$ for a silica particle) based on the resolving/magnifying power of the Bureau of Mines microprojector apparatus (Brown *et al.*, 1938) and for particles with $d_{p,i}$ greater than 5 μm ($d_{AE,i} > 8.1 \mu\text{m}$ for a silica particle) based on the counting rules employed by Hatch (1947). For particles with $d_{p,i}$ between 0.75 and 5 μm , the impinger/microscopy measurement efficiency was calculated according to equation (4), obtained by nonlinear regression ($r^2 > 0.999$) of the experimental data for impinger collection efficiency of silica particles reported by Davies *et al.*, (1951).

$$\epsilon_{i,i} = 0.563 + \frac{1.174}{d_{AE,i}} - \frac{1.760}{d_{AE,i}^2} + \frac{1.194}{d_{AE,i}^3} \quad (4)$$

Finally, each of the individual particle masses calculated from equation (1) and counts calculated from equation (2) were totalled for the 100 000 virtual particles and ratioed to derive the conversion factor (CF) for that sample, as per equation (5):

$$CF \left(\frac{\mu\text{g}/\text{m}^3}{\text{mppcf}} \right) = \frac{\sum_{i=1}^{100,000} M_i(\mu\text{g})}{\sum_{i=1}^{100,000} N_i(\text{particles})} \times \frac{10^6 \text{ particles}}{\text{ft}^3} \times \frac{35.3 \text{ ft}^3}{\text{m}^3} \quad (5)$$

The performance of the simulation algorithm for the CF was assessed by comparison to a set of CFs for mineral dusts obtained directly from side-by-side sampling with impinger sampling/microscopic analysis and cyclone collection/gravimetric analysis as reported

by Tomb and Haney, 1988. The measured CFs and those calculated using our simulation algorithm were not statistically different by paired *t*-test, $P = 0.79$ (Supplementary Table S1, available at *Annals of Work Exposures and Health*).

The archival particle count concentrations (mppcf) were then converted to modern measures of RQ ($\mu\text{g m}^{-3}$) using our conversion factor of 157 derived from the simulations, along with the percent quartz (%Q), as shown in equation (6). The percent quartz in this equation was taken from the values reported by Hatch *et al.*, (1947), as shown in Table 2. Hatch determined the quartz percentage of 39 samples of airborne and settled dust by X-ray diffraction analysis after removal of particles greater than 5 μm .

$$RQ(\mu\text{g} / \text{m}^3) = 157 \times \text{mppcf} \times \%Q + 100 \quad (6)$$

Respiratory protective equipment

The use of respiratory protective equipment (RPE) by workers can be an important exposure modifier in constructing the JEM. Hatch *et al.* (1947) anecdotally noted some use of RPE in this industry; however, the RPE in the past was commonly ¼-mask gasketed metal facepiece air-purifying respirators with electrostatic felt or electret filters. Those respirators tended to provide poor fit quality and there were no formal RPE programs or any indication of fit testing in the distant past in the industrial sand industry. Furthermore, the electret filters of the past have been shown to be unreliable, losing filtration capacity when exposed to water, oil mists, certain organic solvents, and high dust loadings (Revoir and Bien, 1997). Thus, exposures before the 1970s were not adjusted for RPE.

Table 2. Historical industrial sand particle count measurements (Hatch *et al.*, 1947) converted to RQ concentration.

Department, area, or activity	# samples	Particle count concentration		% quartz Mean (SD)	Mean converted $\mu\text{g m}^{-3}$ RQ
		Range (mppcf)	Mean (mppcf)		
Quarrying	14	0.5–16	4.9	78 (15)	598
Crushing	27	1.2–15	4.0		490
Wet processing	28	0.2–4.7	1.4	54 (16)	119
Moist sand handling and storage	17	0.4–3.2	1.3		110
Driers	58	0.7–100	9.1	52 (19)	745
Drier dept. screens	36	2.0–>170	84		6841
Grading screen house	38	1.0–220	62	58 (28)	5646
Pulverizing sand	60	0.4–77	11	94 (5)	1638
Bagging ground silica	25	5.0–60	20		2937
Bulk loading ground silica	5	1.0–180	91		13430
Bagging sand	2	—	2.6	51 (26)	208
Bulk loading sand	30	0.4–350	49		3893

For most of the data in the modern exposure database, individual samples were flagged for RPE use. The assigned exposure concentration for each flagged sample was reduced by the workplace protection factor, *WPF*:

$$C' = \frac{C}{WPF} \quad (7)$$

Where C' is the RQ exposure concentration adjusted for respirator use and C is the measured environmental exposure level. A *WPF* of 5 was used as the default value in this calculation based on reported workplace protection factors of air-purifying respirators for small particle and vapor hazards (Nicas and Neuhaus, 2004). The combined average exposures (MVUE) of the flagged, adjusted, and unflagged, unadjusted samples were then calculated as the best estimate of exposure, thus incorporating both degree of protection and frequency of use of RPE. Because of the numerous assumptions required to perform the exposure adjustments and estimations, additional estimates based on differing assumptions about past exposures and respirator use and protection were computed in parallel for use in sensitivity analyses. Thus, each cell in the JEM contained five estimates of exposure: exposure with no adjustment for RPE ($WPF = 1$), exposures adjusted for recorded frequency of use assuming $WPF = 5$ and $= 10$, and exposures adjusted for assumed continuous use of RPE with $WPF = 5$ and $= 10$.

For some plants, recording of respirator use in the exposure database was delayed for some time after the institution of a respiratory protection program. In these cases, estimates of frequency of use of respirators for a given job title were obtained from the observed frequency, f , for the time after which the information was included in the exposure database, assuming that it was representative of prior usage patterns. This frequency ($0 \leq f \leq 1$) was then used in conjunction with the assigned workplace protection factor to adjust the average exposure levels as follows:

$$C' = C(1 - f) + C\left(\frac{f}{WPF}\right) \quad (8)$$

This formula was applied to all the exposure data covering the period starting with the estimated start date of RPE use up to the point when RPE was specifically recorded in the exposure database.

Results

Converting particle counts to respirable mass

The results of the CF simulations are shown in Table 1. The CF values range over a factor of about 2.5 and vary both across and within the various process areas;

however, there was no statistically significant difference in CF among the different process areas (ANOVA, $P = 0.29$). The overall average CF based on the simulations is $157 \mu\text{g m}^{-3}$ per mppcf (SD = 42). This value is similar to other reported CFs for mineral dusts (Supplementary Table S2, available at *Annals of Work Exposures and Health*) and is 57% of our original CF of $276 \mu\text{g m}^{-3}$ per mppcf obtained from the deterministic algorithm.

Table 2 presents a summary of the Hatch survey data in particle count concentrations and the equivalent RQ concentrations estimated per equation (6). The table entries are grouped by the same scheme Hatch used in presenting the data in the archival report.

The converted average exposure measures for RQ range from 110 to $13430 \mu\text{g m}^{-3}$. The lowest exposures were associated with the processing of wet sand, whereas dry screening and bulk loading operations showed the highest concentrations. The excessively high dust measures for the screening operations represent worst case scenarios as Hatch noted that the workers spent little time during the workday in the immediate vicinity of the screens where the samples were taken. The extraordinarily high exposures measured in bulk loading operations were primarily due to the loading of boxcars with bulk product, a practice that was eliminated in this industry by the early 1970s. Overall, the converted survey data of Hatch indicate that past exposures in this industry for all areas, including those dealing with wet product, were generally higher than modern exposure guidelines for RQ.

The plant/time/JEM

A total of 399 plant–job combinations were identified among the 21 plants having cases and matched controls and were used in constructing the JEM. Company B's information was considerably more detailed than that of Company A as to the identification of those specific jobs sampled in the exposure databases and those held by the study subjects according to their job histories. The number of uniquely identified jobs per plant from Company A ranged from 7 to 10 with an average of 9. In contrast, the numbers of jobs identified per plant from Company B ranged from 6 to 81 with an average of 31.

For purposes of presenting the results of the JEM, which contained thousands of individual plant/job/year combinations, the 399 plant/job combinations were collapsed into 11 major processes or activities (Fig. 1): nonexposed, administrative/technical, mining, crushing, wet processing, drying, sizing/screening, milling, bagging, bulk loading, and maintenance. The overall average unadjusted exposures across time for the 21 plants by major process areas or activities are summarized and

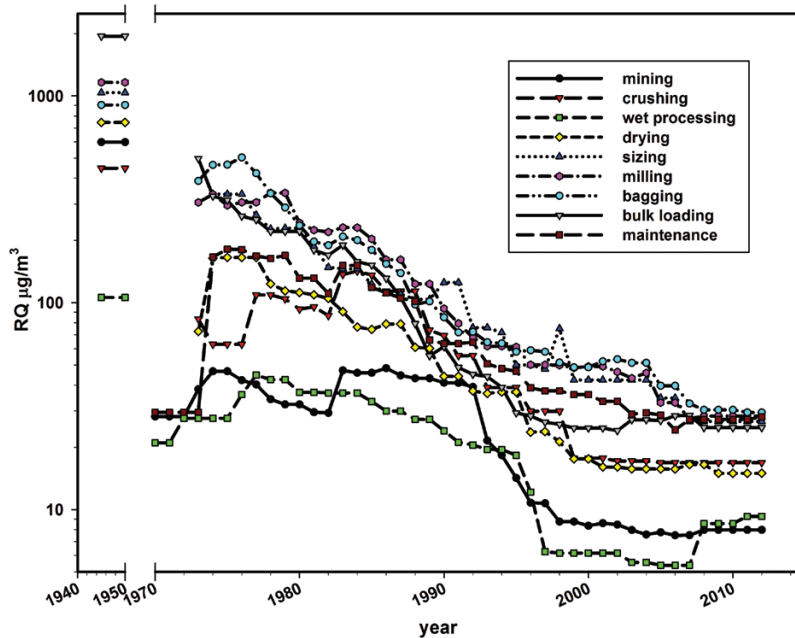


Figure 1. Industry-wide average exposures to RQ for major processes or activities, unadjusted for respiratory protection.

shown in Fig. 1, all unadjusted for RPE ($WPF = 1$). The administrative/technical and nonexposed groups are not included in the figure as the former appeared infrequently in the study subjects' work histories and exposure estimates for the latter were all zero.

Fig. 1 illustrates a profound decrease in exposure levels from the distant past to the beginning of the modern era in the early 1970s for most processes and activities, the one exception being bagging operations. The general decrease over time then continued into the modern era for all process/activity average exposures, all of which, including bagging, dropped below $100 \mu\text{g m}^{-3}$ RQ by the mid-1990s. The overall industry-wide geometric mean of the average RQ exposures before the 1970s, unadjusted for RPE, is $678 \mu\text{g m}^{-3}$, with a range across major activities/processes of 106 to $1945 \mu\text{g m}^{-3}$ (wet processing and bulk loading, respectively). This value dropped to around $148 \mu\text{g m}^{-3}$ in the 1970s, and then to about 103 , 36 , and $19 \mu\text{g m}^{-3}$ in the 1980s, 1990s, and 2000s, respectively. The GM exposure by the 2000s is less than 1% of that from the distant past and about 13% of that from the 1970s.

Fig. 2 presents the 21-plant average frequencies of respirator use during the post-1970 era by major process area. The earliest recorded use of RPE was in 1973 for process areas with historically high exposures such as bagging, milling, and crushing operations. By the late 1970s, RPE was being used in all major process areas

or activities in at least some of the plants. In many of the plants, RPE use became continuous and mandatory for some process areas with traditionally high and difficult to control exposures such as bagging. By the 2000s, frequency of RPE use declined industry-wide, probably because the prevailing exposure levels dropped below the then OSHA PEL ($\sim 100 \mu\text{g m}^{-3}$ RQ).

The distributions of accumulated exposure dose to RQ up to the point of first indication of radiographic silicosis for cases and their matched controls are shown in Fig. 3. Results are presented for unadjusted exposure as well as for exposure adjusted for estimated frequency of use and efficiency of respiratory protection assuming $WPF = 5$ and 10 .

The median unadjusted exposure dose for the cases was $3764 \mu\text{g m}^{-3}$ year and ranged from 221 to $25121 \mu\text{g m}^{-3}$ year. Likewise, for the controls, the median and range were $1595 \mu\text{g m}^{-3}$ year and 0 to $16446 \mu\text{g m}^{-3}$ year. All 67 cases spent at least part of their careers up to point of silicosis identification in jobs with some exposure to RQ, whereas 14 out of 167 matched controls (8.4%) were only in jobs with no exposure. Overall the unadjusted exposure doses for cases and controls were highly significantly different, $P < 0.001$ by Mann-Whitney Rank Sum test.

Accounting for respiratory protection had modest effect on the estimated exposure doses for cases and controls. For the cases, the median exposure doses adjusted

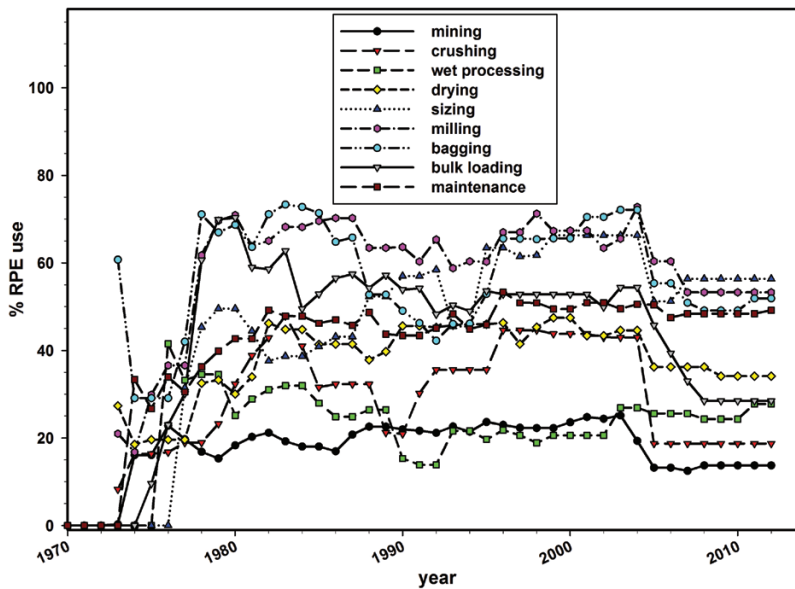


Figure 2. Reported frequency of use of respiratory protective equipment industry-wide for various major processes or activities.

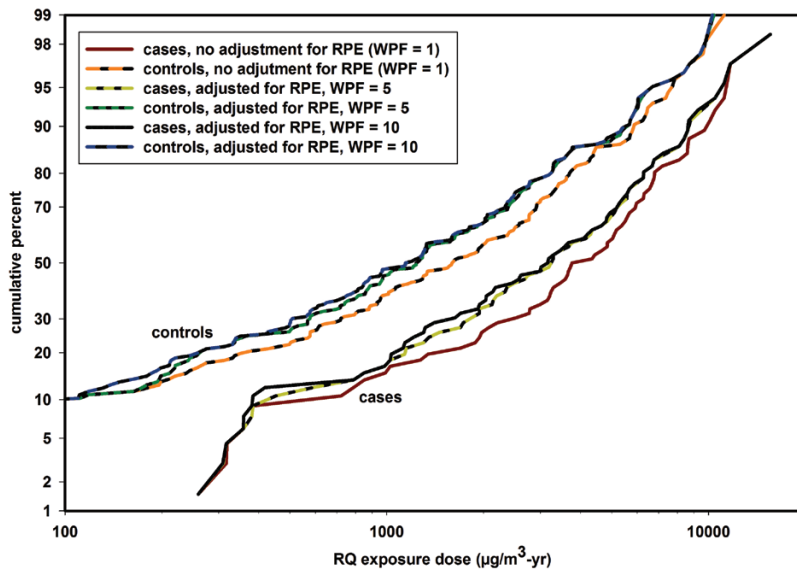


Figure 3. Distributions of estimated RQ exposure dose at first identification of silicosis for cases and controls, with and without adjustment for frequency of use and efficiency of respiratory protective equipment.

for RPE use were 86% and 84% of the unadjusted value assuming $WPF = 5$ and 10 , respectively. For the controls, the respective values were 77% and 72%. With the default WPF value of 5 , the equivalent effective protection factors were only 1.2 and 1.3 for cases and controls, respectively.

The study subjects had an average exposure start date of 1961 and out of 234 total study subjects, 173 (74%) had a hire date before 1970. The percentages of pre-1970 hire for the cases and the controls were very similar (78% and 73%) and were not statistically different. Thus, the cumulative exposures are primarily related to the high

exposures of the distant past when respiratory protection was nonexistent or unreliable. Fully 43% of cases and 50% of controls were always in jobs without respiratory protection and the proportions were not significantly different ($P = 0.69$, χ^2 test). The adjusted exposures assuming WPF of 5 or 10 were also very similar, with a difference of only 6.2% in median adjusted exposure.

Discussion

Retrospective epidemiologic investigations of worker health in industries processing silica-containing minerals, including this work and others for industrial sand (Sanderson *et al.*, 2000; Rando *et al.*, 2001; McDonald *et al.*, 2005; Brown and Rushton, 2005), face a variety of challenges related to exposure assessment. Historical exposure information is often limited or missing and Hatch's archival exposure survey reports are the only exposure data for industrial sand production prior to the 1970s. These data, used in our previous (Rando *et al.*, 2001) and current work as well as that of Sanderson *et al.*, (2000), were in the form of particle count concentrations and were converted into RQ concentrations for use in the JEM.

Count to respirable mass conversion factors for siliceous mineral dusts have been reported in other retrospective epidemiologic and exposure studies (Jacobson and Tomb, 1967; Sutton and Reno, 1968; Ayer *et al.*, 1973; Samimi, 1973; Davis *et al.*, 1983; Sheehy and McJilton, 1987; Montgomery *et al.*, 1991; Seixas *et al.*, 1997). The values of these CFs have ranged over about an order of magnitude (~ 18 to $180 \mu\text{g m}^{-3}$ per mppcf) but most are clustered around an overall average value of approximately 130 (Supplementary Table S2, available at *Annals of Work Exposures and Health*). Sanderson *et al.*, (2000) utilized a CF for industrial sand of 100 that was derived from studies of Vermont granite sheds (Sutton and Reno, 1968; Ayer *et al.*, 1973) and of taconite production (Sheehy and McJilton, 1987). In contrast, we utilized archival particle size data from several industrial sand plants to develop a sand industry-specific CF. Particle size distributions can vary across differing industries, so an industry-specific CF for respirable dust is clearly preferable.

In our original work (Rando *et al.*, 2001), a CF of 276 was developed from a deterministic algorithm using archival particle size distribution data. This value is in the upper range of CFs reported for mineral dusts and may have been positively biased by imprecision of low particle counts observed in the larger particle size categories. In this current work, we applied a stochastic algorithm with log-normal modeling of the particle size distributions rather than using the actual size-categorized particle count data. The current simulation algorithm was

evaluated against directly measured CFs from paired sampling/analysis with impinger/microscopy and respirable dust cyclone/gravimetry (Tomb and Haney, 1988) and our simulation algorithm produced CFs that were on average within 20% of the directly measured values with no statistical difference (Supplementary Table S1, available at *Annals of Work Exposures and Health*). Furthermore, our CF of 157 falls in the middle of the range reported for siliceous dusts and is identical to the value previously suggested by the ACGIH (ACGIH, 1979).

Accounting for the use of RPE in quantitative exposure assessments is another challenge and other investigations of past exposures in the sand industry, both in the USA (Sanderson *et al.*, 2000) and in the UK (Brown and Rushton, 2005), have noted the potential impact on estimated exposures, but made no adjustments for RPE. Quantitative information on RPE effectiveness and use is often unavailable, especially for the distant past, and there is wide variability in protection among workers using the same equipment as well as within individual workers from day to day (Nicas and Neuhaus, 2004). Furthermore, pre-1970 RPE often exhibited poor performance of construction and filtration materials. Robust respiratory protection programs were also uncommon during that time period.

Because of these issues with past RPE use, we chose not to adjust exposures prior to about 1970 for any respiratory protection. After about 1970, exposure estimates were adjusted for the frequency of use and, for purposes of comparison and sensitivity analyses, were computed assuming no RPE and assuming continuous use as well. Our sensitivity analyses of exposure adjustments for RPE showed only modest effect on the overall estimated cumulative exposures in our study population. This modest effect is attributable to much higher unprotected past exposures for the study subjects, 74% of whom began work before 1970. Similar results, also attributed to higher exposures and poorer protection in the distant past, were observed in a study estimating cumulative organic solvent exposures for painters (Wang *et al.*, 2011).

With or without adjustment for RPE, there have been very significant reductions in RQ exposures over time in this industry. In our previous work investigating cancer mortality in 9 industrial sand plants (Rando *et al.*, 2001), similar reductions across time were observed but this current work expands the exposure assessment to 21 plants and extends the time frame of the analysis out another 15 years. Sanderson *et al.*, (2000) also observed similar exposure reductions in 18 American industrial sand plants up to 1996: overall GM dropped from $51.2 \mu\text{g m}^{-3}$ RQ in the 1970s to $7.5 \mu\text{g m}^{-3}$ by the 1990s, a decrease of about 85%. Brown and Rushton (2005) also report

significant exposure reductions in seven industrial sand plants from the UK during a similar time frame (1978–2000). There, exposures declined from 80 $\mu\text{g m}^{-3}$ in the early 1980s to 40 $\mu\text{g m}^{-3}$ by the late 1990s.

Decreases in RQ exposures of US industrial sand workers were driven in part by the establishment of the OSHA/MSHA in the early 1970s and probably by subsequent periodic reductions in recommended exposure guidelines such as the ACGIH TLV. Thus the sand industry accelerated implementing dust control programs that had been ongoing for several decades after the Hatch survey of 1947. Controls included wet drilling equipment in quarries, air conditioned/filtered control booths for dusty operations like crushing, air conditioning/filtering of mobile equipment cabs, eliminating steam coil dryers, drying sheds and some bulk loading operations, ventilation and dust suppression on screens, local exhaust ventilation and air curtains on bagging machines, and replacing burlap product bags having sewn closures with paper or plastic bags sealed with glue or weld lines. Formal RPE programs started in the late 1970s and further reduced the exposure burden for industrial sand workers.

This work had several limitations. Pre-1970 exposures had to be estimated from limited archival data which lacked plant-specific information, except for three plants, so that industry-wide exposure estimates were used for 18 of 21 plants. The archival particle count concentration data also had to be converted to modern measures of RQ. The CF used in this work was based on a small set of archival particle size distribution data, although it was industry-specific. Likewise, the quartz content of dust from the past was estimated from assays of suspended and settled dust reported in the archival surveys, but the quartz content of respirable dust in this industry has changed over time. Work histories for the study subjects were generally complete for recent time periods but more often contained missing information for the distant past. Finally, various assumptions had to be made regarding use of RPE and its effectiveness; although sensitivity analyses suggested that accounting for RPE had only modest effect on the exposures. These various limitations have likely resulted in some misclassification error in the exposure estimates; however, this error likely affected cases and controls equally and nondifferentially.

Conclusions

With the recent (2016) revision of the OSHA PEL for crystalline silica, there is renewed interest in evaluating risk of silicosis from occupational exposures. The industrial sand industry deals with high-purity quartz sand

and has been the subject of several previous mortality studies of silicosis, lung cancer, and kidney disease. In this work, RQ exposures were retrospectively estimated for 67 radiographically-identified silicosis cases and 167 matched controls from the industrial sand workforce, most of whom started work before 1970 and as early as 1929. The JEM was constructed by integrating archival particle count exposure data, converted to equivalent levels of RQ, with an extensive modern (post-1970) exposure database and demonstrated an industry-wide decrease in prevailing exposures to RQ of up to 2 orders of magnitude from the distant to the recent past. Adjustment for use of respiratory protection showed only modest reductions in estimated exposure—a result of most of the accumulated exposure occurring in the past when respiratory protection was rare and unreliable. Overall the estimated cumulative exposures for silicosis cases and controls were significantly different, with the median cumulative exposure for cases being more than twice that of their matched controls.

Supplementary Data

Supplementary data are available at *Annals of Work Exposures and Health* online.

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Conflict of Interest

Funding for this project was provided by the National Industrial Sand Association (NISA). Robert Glenn was employed by NISA from 1988 to 2004, prior to the time the project was funded. The authors declare no other potential conflict of interest relating to the material presented in this article.

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